



## A STUDY ON THE EXAMINATION OF THE SINTER METALLOGRAPHIC STRUCTURE

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Sintering process is carried out domestic and imported iron ore powders, fluxes, coke dust, metallurgical recycling powders and slag forming agents. Nowadays, in order to obtain process and operating parameters that will work with the best sinter quality, extensive researches have been made by iron and steel industry. Sinter quality parameters followed by the sinter blend loaded on the sinter strand and then granulated were examined. We can obtain chemical analysis of the phases by scanning electron microscopy (SEM) technique, but full consistency with images is not always possible and especially SFCA (silico-ferrite of calcium and aluminium) and SFCA-I phases are difficult to distinguish from each other and future studies are required in this field. The mineralogy and microstructure of the sinter plays an important role in determining the physical and metallurgical properties of the iron ore sinter. Mineralogical characterization of sinter phases; it is a complementary tool to conventional physical and metallurgical tests applied to iron ore sinter to evaluate and estimate sinter quality. Measurement techniques used in this study; optical image analysis and X-ray diffraction (XRD), scanning electron microscopy (SEM), energy distribution spectroscopy (EDS), results from raw data converted to autoquan format will be explained on the new studies on the interpretation of the Rietveld system. Depending on the measurement objectives of each technique, the quantification of the crystal phases, the relationship between the measurement results, the chemical composition of the phases and the relations between the minerals, as well as their advantages and disadvantages will be explained.

*Key Words:* Iron ore sinter mineralogy, agglomeration, crystal structure, SFCA, phase chemistry

#### 1. Introduction

Sinter, which is formed by melting of fine iron ores and fluxes (limestone, dolomite, etc.) at high temperature (950-1350°C), is the main ferrous input material of blast furnace. Iron ores constitute sinter cake compound in SFCA phase compound and in the form of glassy structure. Due to the significant effect of SFCA on sinter quality, it is the most important component of the sinter bond matrix. Sinter reactions become successful by controlling the microstructure and concentration of SFCA during the sintering process. In the current existing sinter plants, quality is monitored on the basis of small basicity (CaO/SiO<sub>2</sub>) ratio only. This study will investigate the effect of these four components CaO, Al<sub>2</sub>O<sub>3</sub>,

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Fe<sub>2</sub>O<sub>3</sub>, SiO<sub>2</sub> within the sintering process on the hardness, reducibility and efficiency will be investigated and establish an association.

The literature includes studies that qualitatively examined the microstructure of the sinter in general; and its chemical structure, mineralogy, morphology as well as the distribution of different mineral phase structures in the sinter matrix during the sintering process [1, 2, 7]. Sinter mineral formation mainly consists of SFCA, SFCA-I and SFCA-II phases. The key binding phases that provide strength of the material are SFCA and SFCA-I [3, 6, 12, 13]. The formation and contents of these structures vary according to the operational practices (sinter blend used, temperature, basicity, sintering time, etc.). Our study investigates the mineralogical conditions that allow for the formation of SFCA and SFCA-I phase structures which affect quality especially in the internal structure of the sinter. When the sinter blend consisting of iron ore, limestone, coke dust and flux mixture is heated in a sintering machine, dicalcium ferrite (C<sub>2</sub>F-2CaO.Fe<sub>2</sub>O<sub>3</sub>) structure is formed as the first product at 750-780 °C, and then, iron oxide, SFCA and silicate phases are formed at 1220-1300 °C [4,8,14,15]. With increased sintering temperature, dicalcium ferrites react with hematite to take the form of calcium ferrite (CF-CaO.Fe<sub>2</sub>O<sub>3</sub> [5, 10, 16]. Quartz begins to react with the SFCA-I and SFCA form at 1050°C. SFCA-I breaks down between 1220 °C and 1240 °C and takes the form of SFCA [9, 10, 14, 20].

A study by Scarlett et al. (2004) suggests that the phase compositions in the sinter matrix structure consist of iron oxide by 35 to 60%, ferrites (mostly SFCA) by 20 to 45%, glassy phases by more than 10% and dicalcium silicates by more than 10%. They emphasize that the bond phase morphology is typically composed of SFCA phase composition as well as iron oxides and silicates, forming the most important bond phase structure since SFCA has a major impact on the technological properties of the sinter [17, 18, 21]. Cores et al. [19, 25] consider that the technological quality of the sinter depends on the mineral phase form generated during the sintering process, and SFCA is the strongest bond phase affecting the sinter quality. During studies on the effects of ore mixtures of different compositions on sinter quality, it has been observed that the reducibility and cold strength of the sinter depends on the presence of calcium ferrite in the microstructure of the sinter [20, 34]. The said studies also suggest that the form consisting of hematite cores surrounded by SFCA-I is the desired structure for high sinter quality. During the reduction reactions, the porous structure of the acicular SFCA has been proven to provide a wide surface contact to prevent spread of cracks.

Pownceby and Clout (2003) investigated the initiation of mineral compositions of the SFCA phase and the issue that CF<sub>3</sub> (CaO.3Fe<sub>2</sub>O<sub>3</sub>), CA<sub>3</sub> (CaO.3AI<sub>2</sub>O<sub>3</sub>) and C<sub>4</sub>S<sub>3</sub> (4CaO.3SiO<sub>2</sub>) or Fe<sub>2</sub>O<sub>3</sub>-AI<sub>2</sub>O<sub>3</sub>-CaO compounds can be designed to create a link within a planar structure. In the aforementioned study, they observed the SFCA composition encountered in industrial sinter and named the SFCA forms as SFCA, SFCA-I and SFCA-II (dendritic) solid solution series [3,9,10,22]. In their study, Bristow and Waters (1991) state that SFCA affects the grain structure of the sinter matrix by stabilizing a fine porosity during a reduction in the initial reduction phase. They noticed that the SFCA content in the sinter structure has a maximum effect on the increase of reducibility. They studied on the association between the availability of SFCA and hematite in the sinter cake and maximum reducibility [9, 27, 28, 29].

Industrially produced iron ore sinters include two types of SFCA categorized in the literature based on the composition, morphology and crystal structure of the SFCA phase structure in iron ore. SFCA, which is the first type of these phases in the sintered material is found in the composition of M14O20 stoichiometry and Ca<sup>+2</sup><sub>2.3</sub>Mg<sup>+2</sup><sub>0.8</sub>Al<sup>+3</sup><sub>1.5</sub>Fe<sup>+3</sup><sub>8.3</sub>Si<sup>+4</sup><sub>1.1</sub>O<sup>-2</sup><sub>20</sub>, and the second type SFCA-I is found in the composition of M20O28 stoichiometry and Ca<sup>+2</sup><sub>3.18</sub>Fe<sup>+3</sup><sub>1.548</sub>Al<sup>+3</sup><sub>1.34</sub>O<sup>-2</sup><sub>28</sub> [2,3]. Sinter material differs from chemical composition depending on the raw material used, process conditions and production

conditions. The chemical morphology and element structure of the sintered material, which has a heterogeneous structure, can vary depending on the raw material supply system and process conditions [11-16, 31, 33]. The impact of the SFCA and SFCA-I phases on the formation mechanisms and the formation of a number of sintering parameters have recently been partially done by few studies [19, 23-25, 32]. However, the SFCA phase within the sinter has a significant impact on the improvement of sinter quality parameters such as TI (Tumbler index / cold strength), RDI (Reduction degradation index / hot strength), RI (Reduction index / reduction property) and RUL (Reduction under load) (26, 27, 30).

Sintering plants in the integrated iron and steel plants in our country (İskenderun Iron and Steel Works Co. / ISDEMİR, Ereğli Iron and Steel Works Co. / ERDEMİR and Karabük Iron and Steel Works Co. / KARDEMİR) monitor quality on the basis of small basicity (CaO/SiO<sub>2</sub>) ratio only. The total annual sinter production of these plants exceeds 11 million tons. However, what is important in determining the quality in the sintering process is the fact that the changes in ferrite structures, wustite (FeO) and aluminate cannot be monitored since no common monitoring method could be developed yet. By controlling the SFCA (silico-ferrite calcium and aluminium) structure in the sintered structure, this quaternary phase matrix (CaO, Al<sub>2</sub>O<sub>3</sub>, Fe<sub>2</sub>O<sub>3</sub>, SiO<sub>2</sub>) will be taken under control and all parameters that may affect the quality of the process will be examined. All compounds in the sinter matrix must be evaluated individually using the Rietveld method (Fe<sub>2</sub>O<sub>3</sub>, Fe<sub>3</sub>O<sub>4</sub>, Ca<sub>2</sub>SiO<sub>4</sub>, SFCA, SFCA-I) to know the quantitative contents of existing phase structures. Data obtained after determination of SFCA quantity in the sintered material will be associated with other quality parameters the usage efficiency of the sinter and consequently reduce the raw material costs.

#### 2. Material and Method

Sinter is an important blast furnace input material formed by adding 0-10 mm iron ores and fluxes which cannot be charged directly to the blast furnaces and limestone powder, dolomite, olivine, coke dust, return dust and waste materials (chimney dust, steelmaking slag, mill scale, gas cleaning sludge of blast furnace and steelmaking) in certain proportions without being completely melted, which are heated to 950-1350 °C so as to adhere to each other due to superficial melting. The flow chart of a typical industrial sinter plant is displayed in Figure 1. During the sintering process, the combustion that starts in the sinter furnace moves from the surface of the blend laid on the sinter strand to its base, and the surfaces of the particles in the combustion zone reach the melting temperature, and the gangue components form a semi-liquid slag, the moisture in the blend evaporates, the carbonates decompose, the sulphurous compounds oxidize and their sulphur burns away from the system.

The internal structure of the sinter consists of the composition of iron ores in the sintering process, SFCA and dicalcium silicate, and glassy structure. The reactions that occur also regulate the volume fraction of each mineral that may affect the quality of the sinter, thus the performance of the blast furnace. SFCA is considered to be the most important component of the sinter bond matrix since it affects sinter quality significantly if the content of SFCA in sintered iron ore is high. Sinter reactions become successful by controlling the microstructure and concentration of SFCA during the sintering process. In this study, sample variety was provided by producing at different operating parameters with a laboratory type sintering machine in order to be able to perform more rapid test studies from iron ore blends prepared in different compositions. In sinter production, domestic and imported iron ores are mixed with certain proportions of fluxes (limestone, dolomite, etc.) and fuel (coke dust) to produce sinter in the basicity values of 1.6-2.0 (CaO/SiO<sub>2</sub>) and at different operating parameters. Ratios of

imported iron powder and domestic iron powder to be used in the sinter blend will vary between 50-70% and between 30-50%, respectively depending on operating and laboratory practices. The content of fluxes to be used in the sinter blend will be in the range of 7 to 9% depending on the acidic compounds such as  $SiO_2$  and  $Al_2O_3$ .



Figure 1. Typical flow chart of industrial type sinter production [35].

Sinter blend samples were prepared in accordance with the following parameters; • Consumption of coke dust. It will vary between 6% and 7% in the blend depending on the sintering temperature.

- Humidity of the raw material: 7-8%.
- Ignition temperature: 1000~1200 °C, 1 minute ignition negative pressure: 5660 Pa.
- Negative pressure for sinter: 10.850 Pa.

## **3.** Experimental Studies and Comments

## 3.1. SEM and XRD Studies on Sinter Samples

Given the increasing importance and studies in directing the sinter production quality according to the SFCA content in the sinter phase structure in addition to the existing physical and chemical quality monitoring tests of the sinter, which is an important input material in blast furnace process control; determination of ideal SFCA will help to control all sintering parameters of the sinter, which is the main input material of the blast furnace process in iron and steel plants. Thus, besides the cost advantage to be created by a better process control by charging more stable sinter to the Blast Furnace, a new iron production quality monitoring will be provided for the iron and steel industry on a global scale. Quadruple bond SFCA phase has been accepted as a main parameter in the sintering process by scientists since it significantly affects the technological quality of the sinter including high mechanical hardness (TI, RI and RDI, etc.), but it has not been sufficiently studied yet. Studies conducted on the effects of microstructure and mineral composition on the crack resistance of the sinter noticed that SFCA-I (especially acicular SFCA) is the main material affecting the spreading resistance of cracks. It has been observed that the acicular SFCA type of porous structure provides a greater reaction area in solid-gas contact, thereby increasing the reducibility in the blast furnace, shortening the processing time and saving fuel (metallurgical coke) and time.



Figure 2. Sinter sample a) S-1 and b) S-2 SEM images, c) S-3 and d) S-4 optical microscope images (Hem: Hematite, Mag: Magnetite, SFCA, SFCA-I (X500)

SEM and optical microscope studies were performed with 500X magnification on sinter samples. The presence of SFCA and SFCA-I phase structures in the sinter matrix varies depending on the sintering temperature, blend ignition time and furnace temperature. The SEM and optical microscope images of the sinter samples are indicated in Figure 2.





XRD phase diagram was demonstrated in Figure 3. During the XRD studies conducted,  $Fe_2O_3$  (hematite),  $Fe_3O_4$  (magnetite), FeO (wustite), SiO<sub>2</sub> (quartz), Ca<sub>2</sub>SiO<sub>4</sub> (larnite), CaO (lime), and XRD device printouts for SFCA and SFCA-I phases are quantitatively determined with the help of the Rietveld Method. The composition information of SFCA and SFCA-I phases stoichiometrically is demonstrated in Table 1.

Table 1. Stoichiometric composition information of SFCA and SI	FCA-I phases
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	Fe <sup>+3</sup>	Fe <sup>+2</sup>	Fe	Al	Са	Mg	Si	Mn
SFCA (M <sub>14</sub> O <sub>20</sub> )	10.18	0.90	11.08	0.50	1.85	0.17	0.49	0.08
SFCA-I (M <sub>20</sub> O <sub>28</sub> )	14.36	1.72	16.08	0.38	3.48	0.21	0.05	0.38

## 3.2 The Study of Rietveld Method and Autoquan Program on the Sinter Samples





The phase structures in the sinter were determined using XRD devices with X-Ray tubes that irradiates Cu K-alpha and Co K-alpha. The scanning process was done between 5-90° at the scanning speed of 2 degree/min. Crystal data phase files with \* .XRDML extension of sinter samples is created in XRD device and these files are converted to files with \*.RD extension by PANalytical X'Pert Highscore Plus software program. In this file, the files are converted to \*.RAW files using ConVX.exe program and opened with the Autoquan program having the crystal data files of the related phases.

Autoquan program and the rietveld method can be used to determine the individual percentage of all phases in the sinter structure. Data on quantitative contents of existing phase structures is obtained from the study conducted by this method. The XRD drawing of a typical sinter material is given in Figure 4. The position of the peaks obtained from the crystal structure of the sinter is shown as a vertical line. For example, the hematite mineral content in the sinter material can be easily identified and measured by XRD with an approximately 12 minute scan. Rietveld image of the sinter sample was indicated in Figure 4. When using powder XRD with mineral compositions obtained by SEM analysis, much information can be obtained about the element distribution in various minerals. The advantage of this method over other methods is to more accurately determine phase contents (%) by using the information content of the diffractogram better.

Before the raw data obtained were evaluated in Autoquan, the conditions of the relevant device were kept available in the device file. This step was important for a proper refinement process. However, the XRD convert program used to convert the raw data format to Autoquan format is given in Figure 5.

File(s) to Convert	
File Type : Philips VAX RD	Select File(s) (none selected)
Output file details	Output Parameters
File Type ASCII 2theta,I	Convert whole file (s)
	Start Angle : 0,000
	End Angle : 0,000
Ensure unique filename : 🔽 Suffix :  b	Count Time: 100
Directory : F:\XRD Convert\ConvX\	
Change Directory	Anode:
	Wavelength:
Date of output file	Alpha-2 stripped :
Date of input file	Alpha-2 ratio : 0,50000
l oday's date	

#### Figure 5. XRD convert program

Figure 5 indicates charts containing the results of quantitative phase measurements using Autoquan with an X-Ray tube that radiates Cu K-alpha and Co K-alpha. Different SFCA values were found in the same samples subjected to Cu K-alpha and Co K-alpha analysis. According to the results obtained with the tube that radiates Cu K-alpha during the investigation of the phase structures of the sinter materials, since the incident ray is absorbed due to the fluorescence and absorption effect, especially in iron-containing materials, the intensity/counts sensitivity values were quite low, so no healthy results could be obtained. In order to determine the phase structures in the sinter, XRD device with X-Ray tube that radiates Co K-alpha, which can make more precise measurements in iron-containing phases, was preferred. After the sample size was grinded to 20 microns, it was scanned at 30 kV and 35 mA in the XRD device. Figure 6 reveals the quantitative (%) sinter phase results of the structures in the internal morphology of the sinter sample, obtained by Rietveld analysis performed via the Autoquan program using XRD device with Cu K-alpha and Co K-alpha radiation on the sinter samples.

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Figure 6. Rietveld analysis quantitative sinter phase results by XRD device with Cu K-alpha and Co K-alpha radiation.

Using the rietveld method, all compounds in the sinter matrix are evaluated individually (FeO, Fe<sub>2</sub>O<sub>3</sub>, Fe<sub>3</sub>O<sub>4</sub>, Ca<sub>2</sub>SiO<sub>4</sub>, SFCA, SFCA-I, etc.) to know about the quantitative contents of the existing phase structures. The Rietveld method utilizes the relative weight ratios of all phase crystals included in the model better and helps the determination of more accurate phase quantities (as %), and results are achieved quantitatively and quickly in a few minutes without the need for standard or calibration [22, 30, 31]. It also facilitates the interpretation of sinter phase data and the regular protection of phases. The Autoquan program supports the analytical listing of SFCA phase results from the sinter sample and

transferring the results to standard applications. Thanks to this program, changes that may occur in the sinter structure or process conditions can be tracked more accurately with the SFCA data.

## 4. Conclusion

All-important parameters in the sinter material, which affect the quality of the sintering process are examined in order to make the sintering process more stable with a detailed internal structure analysis. The changes shown by the structures within the sinter matrix structure, especially SFCA, SFCA-I and SFCA-II phase structures, which have a great effect on the physical and metallurgical properties of the sinter, depending on the sintering temperature, time, raw material type and basicity are followed by Autoquan program and Rietveld method, and the process and raw material conditions required for the full control of the sinter mineral formation are determined to create more durable sinter production and process monitoring systematics. Within the scope of this study, it will be possible to use the data to be obtained with the XRD device to quantify the phase structures formed in the sinter produced using the related software. In this context, it is important to make a correlation with the physical properties of the material, especially the ones that affect the strength of the material, by following up the ratio of iron oxides formed during the process to the SFCA phase structures. The result of the study is reduction in the return dust contents as a result of the production of high-strength sinter, and the valuation of such fine dusts in the blast furnace to provide significant savings in ore consumption. Utilization of an X-Ray tube that radiates Co K-alpha, which can make more precise measurements in iron-containing phases for investigation of the sinter phase structure, is important due to the fluorescence effect at more intensive values.

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